A New Method For Synchronization Of A Simple Chaotic systems

Abdel Abdel-Azeem Mohamed and Samy H. Darwish

Faculty of Engineering, Pharos University, Alexandria, Egypt
Azima65@hotmail.com, and Salord1960@yahoo.com

Abstract

This paper presents a new algorithm for controlling a class of simple chaotic system that contain only one nonlinear term. Chaos synchronization using parametric controllers is generalized for typical simple chaotic systems based on largest conditional Lyapunov exponents. A more robust and rigorous definition can be given in terms of the Lyapunov exponents. When the Lyapunov exponents for system are all negative, the systems will synchronize. The Pecora -Carroll method is one of the methods for synchronizing chaotic systems. However, the method is restricted to select the driving signals or its configuration. The proposed method does not depend on the choice of the drive signal or its configuration; it depends only on the nonlinear coupling term which makes the largest conditional Lyapunov exponents of the response system negative. The comparison between the implementation of presented method and the Pecora –Carroll(PC) method is explained. Simulations are presented graphically to confirm the validity of the proposed method.

Keywords: Chaotic system; Lyapunov exponents, synchronization, Stability

1-Introduction

Chaotic systems have been widely studied by many scientists and engineers from different viewpoints. Chaos is one of the most significant topics in nonlinear science, and has been intensively studying since the Lorenz system [1] was introduced. After many chaotic systems have been discovered and developed, scientists have focused on chaos control and chaos synchronization since 1990s. Chaos synchronization was discovered by Pecora and Carroll [2] and there has been great interest in its applications, such as secure communication, and system identification. Given a chaotic system considered as a master system, and another identical system considered as a slave system, the dynamical behaviors of them may be identical after a transient when the slave system is driven by a control input. There are many methods for controlling chaos such as feedback and synchronization techniques [1-4].
The synchronization of two chaotic dynamical system occurs when the trajectories of one the systems will converge to the other system at the same time or the two systems show the same behavior at the same time. Different methods for synchronization such as complete synchronization, phase synchronization, lag synchronization and generalized synchronizations have been presented [3-6].

To achieve synchronization, there are many methods for linking chaotic systems. Famous two methods are: the linear diffusive coupling, as initially suggested by Fujisaka and Yamada [8 and 9], and driving coupling, introduced by Pecora and Carroll[5-7]. There are another additive coupling which is offered by the open-plus-closed-loop method to control and synchronize chaotic systems developed by Jackson and Grosu[10-12].

Concerning stability, there are two criteria which are most commonly used for stability of synchronized chaotic motions, these two criteria are the Lyapunov function criterion [12,13,17] and the conditional Lyapunov exponents [13-15]. In many practical cases, Lyapunov functions cannot be found, even for systems that possess a stable manifold of synchronized motions for a broad range of parameters of coupled systems, and/or the coupling itself. In contrast with Lyapunov functions, the analysis of conditional Lyapunov exponents [13,14,15] is quite straightforward and can be easily employed, even for rather complicated systems. The presence of synchronization can occur if the conditional Lyapunov exponents of the response system are negative.

Lyapunov exponents are commonly used for chaos identification in nonlinear dynamical systems by showing the average rate of growing or shrinking of a small volume of initial conditions. These exponents provide a quantitative measure for the sensitivity of the nonlinear system to the change of initial conditions. Also Lyapunov exponents demonstrate the chaotic behavior of the system [12, 13], and there are several methods for numerical calculation of Lyapunov exponents [14, 15].

The control of typical chaotic system by synchronization is the aim of this work. Thus a method suggested by forcing the largest Lyapunov exponent of the response system to be negative. This is achieved by combining the open-loop-closed-loop method and Routh–Hurwitz criteria [16, 17].

2. Synchronization
This section reviews the Pecora and Carroll method and introduces the proposed method for synchronization of chaotic system.

2.1 Pecora and Carroll method.
This method is a widely used approach synchronization problem [5-7]. Consider an n-dimensional autonomous system governed by the equation

\[ \frac{dx}{dt} = f(x) \]

\[ x = (x_1, x_2, ..., x_n)^T \]  \hspace{1cm} (1)

the system into two parts in an arbitrary way, i.e. dividing the state vector into \( \mathbf{X} = [\mathbf{x}_D, \mathbf{x}_R]^T \). The \( \mathbf{D} \) is referred to as the driving subsystem, and \( \mathbf{R} \) is referred to as the response subsystem respectively, then
\[ x_D = g(x_D, x_R), \] \hspace{1cm} (2)
\[ x_R = h(x_D, x_R). \] \hspace{1cm} (3)

where,
\[ x_D = (x_1, x_2, \ldots, x_m)^T, \]
\[ x_R = (x_{m+1}, \ldots, x_n)^T, \]
\[ g = \left[ f_1(x), \ldots, f_m(x) \right]^T, \]
\[ h = \left[ f_{m+1}(x), \ldots, f_n(x) \right]^T. \]

Pecora and Carroll suggested building an identical copy of the response subsystem and driving it with the \( X_D \) variable coming from the original system. In such a method, the following compound system of equation can be found
\[ x_D = g(x_D, x_R), \] \hspace{1cm} (4)
\[ x_R = h(x_D, x_R), \] \hspace{1cm} (5)
\[ x_D = h(x_D, x_R'), \] \hspace{1cm} (6)

2.1.1 Theorem 1
The subsystems \( X_R \) and \( X_R' \) will synchronize only if the conditional Lyapunov exponents are all negative [5].

Under the right conditions, the \( x_R' \) variable will converge asymptotically to the \( x_R \) variable and continue to remain in step with instantaneous value of \( x_R(t) \). Here the drive or master system controls the response or slave system through \( x_D \) component. If all conditional Lyapunov exponents of the response system are negative then the synchronization occurs. Otherwise the synchronization does not occur if at least one of the conditional Lyapunov exponents is positive.

2.1.2 Lyapunov exponents

The idea of synchronizing two identical chaotic systems that start from different initial conditions can occur when the largest Lyapunov exponents for the subsystem to be synchronized are all negative. The Lyapunov exponent measures the growth of small perturbation of the difference between two systems. The next paragraph introduces briefly how to calculate the Largest Lyapunov exponents of the whole system after synchronization [13-15].

It is known that under suitable coupling one system will follow another system if its largest conditional Lyapunov exponent is negative. The largest Lyapunov exponents
of the whole system can calculate the distance between the subsystem and the original system which is

\[ \sqrt{N} \sum_{i=1}^{N} \partial^2 x_0(i). \]  

Where N is

With the evaluation of time, the distance will be expanded along the largest eigenvalues directions, so the largest Lyapunov exponents can be obtained as follows

\[ \lambda = \lim_{t \to \infty} \frac{1}{t} \ln \sqrt{N} \sum_{i=1}^{N} \partial^2 x_0(i) \left( \sqrt{N} \sum_{i=1}^{N} \partial^2 x_i(i) \right) \]  

(7)

2.2 The proposed method of Synchronization

Some undesirable characteristics of the Pecora and Carroll method are the existence of the positive conditional Lyapunov exponent and the dependence on the configuration of the drive signal. The proposed method avoids this problem by choosing the values of system parameters that make the largest Lyapunov exponents negative using the concept of Routh- Hurwitz criteria and the dependence on the chosen of drive signal are discarded.

The proposed method depends upon the method of Open- Plus- Closed- Loop for control of dynamical systems (OPCL) [10-12]. which is summarized as follows

Consider the dynamical system is given by:

\[ \frac{dx}{dt} = F(x), \quad (x \in \mathbb{R}^n) \]  

(8)

if one wants to entrain the solution of a dynamical systems to some goal behavior, \( g(t) \), using linear feedback, in order to obtain

\[ \lim_{t \to \infty} (x(t) - g(t)) = 0 \]  

the dynamics is of the form

\[ \frac{dx}{dt} = F(x(t)) + D(t, x, g) \]  

(9)

where, \( D(t, x, g) \) is the drive term and is given by:

\[ D(t, x, g) = \frac{dg}{dt} - F(g, t) + \left( A - \frac{\partial F}{\partial x} \right) (x - g), \]  

(10)

where A is a constant matrix with eigenvalues having negative real part, D is some suitable matrix in this case \( g(t) \) has to be restricted to some solution of

\[ \frac{dg}{dt} = F(g, t) \]  

(11)

The idea of the proposed method is replacing the parameter \( P \) in place of the nonlinear term in the constant matrix of the Jacobian of the master system and choosing the value of the parameter \( P \) that makes the eigenvalues having negative real part and also satisfying the Routh – Hurwitz criteria for stability then derive the slave system by the drive term as follows

\[ (A - \frac{\partial F}{\partial x}) (x - y) \]  

(12)

consider the dynamical system given by:
\[
\frac{dx}{dt} = F(x,t)
\]  \hspace{1cm} (13)

Then the slave system will be:
\[
\frac{dy}{dt} = F(y,t) + (A - \frac{\partial F}{\partial x} \bigg|_{x=y})(x-y)
\]  \hspace{1cm} (14)

Where, \( A \) is a constant matrix with eigenvalues with negative real parts. Then \( x(t) \) converges to \( y(t) \) for any \( \| x(0) - y(0) \| \) small enough.

The proposed method is based on the analysis of the characteristic polynomial coefficients of the matrix \( A \). Let the characteristic polynomial of \( A \) be denoted by:
\[
A(s) = a_n s^n + a_{n-1} s^{n-1} + \ldots + a_0 = 0, \quad a_n > 0
\]  \hspace{1cm} (15)

As presented in [10], it is possible to derive necessary and sufficient conditions for the existence of eigenvalues with negative real part by applying Routh- Hurwitz conditions. By applying these conditions, it is possible to determine the numerical interval of parameter that insure the eigenvalues in the left hand plane

2.2.2 The proposed method

The algorithm of the proposed method is given by
1-Find the Jacobian matrix of the master system \( J = \frac{\partial F}{\partial x} \)

2-Find the matrix \( A \) by replacing the element containing the variable in the matrix \( J \) by the parameter \( P \) (coupling term)

3-Find the characteristic equation of the matrix \( A \)

4-Applying the Routh- Hurwitz criteria to find the range values of \( P \) and substitute it in the matrix \( A \)

5-Find the drive term \( (A - \frac{\partial F}{\partial x} \bigg|_{x=y})(x-y) \)

7-Create the synchronization algorithm according to the range of parameter \( P \) as follows

\[
\text{The master system} \quad \frac{dx}{dt} = F(x,t)
\]

\[
\text{The slave system} \quad \frac{dy}{dt} = F(y,t) + (A - \frac{\partial F}{\partial x} \bigg|_{x=y})(x-y)
\]  \hspace{1cm} (16)

8-Test for the synchronization (calculate the largest Lyapunov exponents) the algorithm is coded in C++

3 Case Study

The following system will be analyzed using the suggested method and the Pecora-Carroll method
3.1 Simple chaotic system

Consider the following system [14] is described by

\[
\begin{align*}
\frac{dx}{dt} &= y + z \\
\frac{dy}{dt} &= -x + 0.5y \\
\frac{dz}{dt} &= x^2 - z
\end{align*}
\]

The system 1 has only six terms, a single quadratic nonlinearity ($x^2$), and two critical points (-2, -4, 4) and (0, 0, 0). The largest Lyapunov exponent of the system is equal to (0.1342) and the chaotic behavior of the system is shown in figure (1)

Figure 1a- the time response of $x(t)$ of system 1

Figure 1b- the phase plane plot of $x(t)$ versus $y(t)$ of system

By applying the concept of The Pecora and Carroll to the system using $y$-drive configuration one can get
The conditional Lyapunov exponents of the subsystem are (-0.17, -.84) i.e. the synchronization occurs. Also the largest Lyapunov exponents of the whole system is 0.102 and the system after synchronization is chaotic. Figure (2) shows the synchronization of the chaotic system in case of y-drive.

\[
\begin{align*}
\frac{dx}{dt} &= y + z \\
\frac{dy}{dt} &= -x + 0.5*y \\
\frac{dz}{dt} &= x^2 - z \\
\frac{dx_1}{dt} &= y + z_1 \\
\frac{dz_1}{dt} &= x_1^2 - z_1
\end{align*}
\] (18)

Figure 2a- The time response of x(t) of the drive system using PC method

Figure 2b- The time response of x_1(t) of the response system using PC method
Figure 2c- The error of synchronization between \(x(t), x_1(t)\) using PC method

Figure 2d- The phase plane \((x(t) \text{ versus } z(t))\) of whole system after synchronization using PC method (non-oscillating behavior)

In the case of synchronization by Pecora and Carroll method the synchronization does not occur and it depends on the configuration for driving signal. For example, in the \(x(t)\) configurations the subsystem does not synchronize, the conditional Lyapunov exponent positive, the Conditional Lyapunov exponent for drive-response systems of systems is shown in table 2.

<table>
<thead>
<tr>
<th>system</th>
<th>Drive signal</th>
<th>Response system</th>
<th>Conditional Lyapunov exponents</th>
</tr>
</thead>
<tbody>
<tr>
<td>System 2</td>
<td>(x)</td>
<td>((y, z))</td>
<td>+ve (no synchronization)</td>
</tr>
<tr>
<td></td>
<td>(y)</td>
<td>((x, z))</td>
<td>-ve (non-oscillating synchronization behavior)</td>
</tr>
<tr>
<td></td>
<td>(z)</td>
<td>((x, y))</td>
<td>+ve (no synchronization)</td>
</tr>
</tbody>
</table>

Table 1- Conditional Lyapunov exponent for system 1 for different drive signals using PC method
The results are in a good agreement with other results that published in [16]. To avoid this problem, the new algorithm can be used for synchronization, the algorithm selects the drive signal directly from the nonlinear part.

By applying the method outlined in section (3) then the master system is given by equation (14) the Jacobian matrix is given by

\[
J = \begin{bmatrix}
0 & 1 & 1 \\
-1 & 0.5 & 0 \\
2p & 0 & -1
\end{bmatrix}
\]  \hspace{1cm} (19)

The coupling terms comes from the matrix

\[
A = \begin{bmatrix}
0 & 1 & 1 \\
-1 & 0.5 & 0 \\
2p & 0 & -1
\end{bmatrix}
\]  \hspace{1cm} (20)

Where \( P \) is a parameter that has to be chosen to make the eigenvalues of \( A \) having negative real parts. The characteristics equation is given by:

\[
\lambda^3 + 0.5 \lambda^2 + 0.5 \lambda + 1 - 2p \lambda + 1.0 p = 0
\]  \hspace{1cm} (21)

With, \( a1 = 0.5, a2 = 0.5 - 2p \) and \( a3 = 1 + p \)

The Routh – Hurwitz conditions are \( a1 > 0, a3 > 0 \) and \( a1 \cdot a2 - a3 > 0 \)

Given the condition \(-2 > P > -0.75\), then the slave system is given by

\[
\begin{align*}
\frac{dx_i}{dt} &= y_i + z_i \\
\frac{dy_i}{dt} &= -x_i + 0.5 y_i \\
\frac{dz_i}{dt} &= (x_i)2 - z_i + (p - 2x)(x_i - x)
\end{align*}
\]  \hspace{1cm} (22)

Figure (3) shows the synchronization of the chaotic system using the proposed method.
Figure 3a- The time response of $x(t)$ of the drive system using the proposed method

Figure 3b- The time response of $x_1(t)$ of the response system 1 using the proposed method

Figure 3c- The phase plane plot of $x(t)$ vs. $y(t)$ the system after synchronization using the proposed method
Figure 3d- The error of synchronization between $x(t)$, $x_1(t)$ using the proposed method

From the previous figures one can notice that synchronization process is archiving without selecting the type of configurations of the drive signal. Also, the error of synchronization in the proposed method is smaller than the method of Pecora–Carroll and the new method does not depend on the configuration of the drive signal also the new method detect the type of synchronization behavior.

Another proof to validate the proposed method by illustrating that in some system the method of PC is not applicable and synchronization not occur with different drive signals but the new algorithm avoids this problem.

The system 2 is described in [14, 16] as:

$$\begin{align*}
\frac{dx}{dt} &= a - y \\
\frac{dy}{dt} &= b + z \\
\frac{dz}{dt} &= x \cdot y - z
\end{align*}$$

This system has six terms, a single nonlinearity ($x \cdot y$), and two parameters $a$ and $b$. Letting $a = 0.9$, and $b = 0.4$, these values lead to the chaotic behavior with largest Lyapunov exponent (0.064). Its time response and phase plane plots are shown in Figure (4)
By applying the concept of the Pecora and Carroll to the system using x-drive configuration one can get

\[
\begin{align*}
\frac{dx}{dt} &= a - y \\
\frac{dy}{dt} &= b + z \\
\frac{dz}{dt} &= x \cdot y - z \\
\frac{dy_1}{dt} &= b + z_1 \\
\frac{dz_1}{dt} &= x \cdot y_1 - z_1
\end{align*}
\]  

The conditional Lyapunov exponents of the subsystem are (0.052, 0.04), i.e. the synchronization will not occur. Also the largest Lyapunov exponent of the whole
system is positive and the system is not synchronized. Also the same result is appears in the case of y and z as a drive signals and the system is not synchronized by the method of Pecora- Carroll. The Conditional Lyapunov exponents for the drive-response systems of systems are shown in table 2.

<table>
<thead>
<tr>
<th>System of equation (23)</th>
<th>Drive signal</th>
<th>Response system</th>
<th>Conditional Lyapunov exponents</th>
<th>Synchronization</th>
</tr>
</thead>
<tbody>
<tr>
<td>x</td>
<td>(y, z)</td>
<td>+ve</td>
<td>no synchronization</td>
<td></td>
</tr>
<tr>
<td>y</td>
<td>(x, z)</td>
<td>+ve</td>
<td>no synchronization</td>
<td></td>
</tr>
<tr>
<td>z</td>
<td>(x, y)</td>
<td>+ve</td>
<td>no synchronization</td>
<td></td>
</tr>
</tbody>
</table>

Table 2- Conditional Lyapunov exponents for the system 2 for different drive signals using PC method

The synchronization not occur for different drive signals using PC method. To avoid this problems the new algorithm can be used for synchronization, the algorithm selects the drive signal directly from the nonlinear part.

By applying the method outlined in section (2) then the master system is given by equation (17) the Jacobian matrix is given by

\[ J = \begin{bmatrix} 0 & -1 & 1 \\ 0 & 0 & 1 \\ 1 & 1 & -1 \end{bmatrix} \]  \hspace{1cm} (25)

The coupling terms comes from the arbitrary matrix

\[ A = \begin{bmatrix} 0 & -1 & 1 \\ 0 & 0 & 1 \\ 1 & p & -1 \end{bmatrix} \]  \hspace{1cm} (26)

Where, P is a parameter that has to be chosen to make the eigenvalues of A containing negative real parts. The characteristics equation is

\[ \lambda^3 + \lambda^2 - P \lambda + 1 = 0 \]  \hspace{1cm} (27)

with a1 = 1, a2 = -P and a3 = 1
The Routh–Hurwitz conditions are $a_1 > 0$, $a_3 > 0$ and $a_1 a_2 - a_3 > 0$

Given the condition $P<-1$, then the slave system is given by

\[
\begin{align*}
\frac{dx_i}{dt} & = 0.9 - y_i \\
\frac{dy_i}{dt} & = 0.4 + z \\
\frac{dz_i}{dt} & = x_i y_i - z_i + (1 - y_i)(x_i - x) + (p - x)(y_i - y)
\end{align*}
\] (28)

Figure (5) shows the synchronization of the chaotic system using the proposed method

Figure 5a- The time response $y(t)$ of the drive system 2 using the proposed method

Figure 5b- The time response $y_1(t)$ of the response system using the proposed method
From the previous figures it can be noted that the synchronization process is achieved without selecting the type of configurations of the drive signal, and the system is synchronized but with using the method of Pecora and Carroll the synchronization does not occur. The proposed algorithm is applicable in some regimes in which the Pecora and Carroll method fail.

4- CONCLUSION
The proposed method for controlling and synchronizing typical simple chaotic system with only one nonlinear term can be achieved without depending on the configuration of the drive signal besides minimizing the error of synchronization. Numerical results verify the validity and effectiveness of the control method.
References